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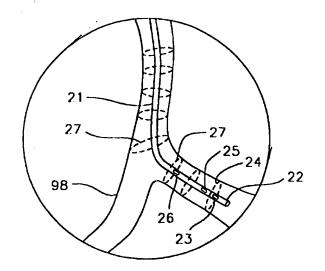
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(54) Title: THREE-DIMENSIONAL INTRALUMINAL ULTRASOUND IMAGE RECONSTRUCTION

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#### (57) Abstract

A method for imaging an organ or internal structure within a body to obtain three-dimensional reconstruction of the organ includes steps of providing an intraluminal ultrasound imaging system (23) capable of obtaining echographic images of the surrounding of a catheter imaging tip (22) located inside the body of a patient. The intraluminal ultrasound catheter imaging tip (22) is positioned within a region of interest (97) inside the body of the patient and a plurality of echographic images are obtained during deliberate movement or pull-back of the catheter (21), each image corresponding to an echographic data set. The position of the catheter axis with respect to each echographic



data set obtained during pull-back is recorded. The recorded position of the catheter tip (22) can be used to calculate a catheter pullback trajectory in three-dimensional space. The images are stacked around the catheter pull-back trajectory by positioning the origin of a first image at a first recorded position, and positioning subsequent images at their respective distances from the first image, wherein each echographic data set is positioned so that the catheter axis is aligned with the catheter pull-back trajectory.

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#### DESCRIPTION

### THREE-DIMENSIONAL INTRALUMINAL ULTRASOUND IMAGE RECONSTRUCTION

This is a continuation-in-part of U.S. Application Serial No. 08/717,153, filed September 20, 1996.

#### Field of the Invention

This invention relates to methods and apparatus for ultrasound imaging within a body cavity or lumen, and more particularly relates to methods and apparatus which enhance the accuracy of three-dimensional (3D) image reconstruction where the 3D image is reconstructed from a series of images taken over a nonlinear path.

#### Background of the Invention

Intravascular ultrasound imaging is now a common technique used to determine the position and characteristics of stenotic lesions in the arteries of a patient. Presently, 3D images of a region of a vessel are generated by acquiring image data from an ultrasound transducer during pull-back of the transducer within a region of interest, and then stacking the sequence of 2D images thus acquired to generate a 3D image. In procedures commonly used, the 2D images are stacked equidistantly along a straight centerline, assuming uniform velocity of pull-back. If pull-back velocity is nonuniform, then the position of each image is registered, and images are stacked at registered positions. Although this non-uniform pull-back does not lead to 3D distortion, it may result in gaps in the image due to nonuniform spacing. These methods assume that the transducer follows a linear path during pull-back, whereas in reality the path is often curved in 3D space. Thus, by making this assumption, substantial error may be introduced into the 3D reconstruction, resulting in an image having significant distortion in the 3D representation of reality. This error results because each

image is assumed to lie in a plane which is parallel to the plane of each adjacent image, whereas the image planes are, in reality, angled relative to one another.

At least one attempt has recently been made to correct for this error by generating a 3D catheter centerline, and then stacking 2D images according to 5 the geometry of the catheter centerline. See Slager et al., The Thorax Center Journal 7/3:36-37 (1995); Roelandt et al., Circulation 90(2):1044-1055 (1994); Slager et al., Journal of the American College of Cardiology, 25:144A (1995); and Laban et al., Thorax Center, University Hospital, Rotterdam, Netherlands, "ANGUS: A new Approach to Three-dimensional Reconstruction of Coronary Vessels by Combined Use of Angiography and Intravascular Ultrasound"; these 10 and all other references cited herein are expressly incorporated by reference as if fully set forth herein in their entirety. According to the Slager method, use is made of a catheter having radiopaque markers, and the catheter centerline is reconstructed from data obtained through bi-plane fluoroscopy before and/or during catheter pull-back. The use of fluoroscopy as a technique for the 15 determination of a 3D centerline is, however, not without certain drawbacks and side effects. Thus, a need exists for apparatus and methods to determine pullback trajectory without using fluoroscopy, so as to permit accurate 3D reconstruction from sequential ultrasound images.

#### 20 Summary of the Invention

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We have discovered methods and apparatus for imaging an organ, lumen, or other internal structure within a body to obtain accurate 3D reconstruction of the organ, lumen, or other internal structure. The methods and apparatus will find applicability to the coronary arteries, arteries generally, and more generally the vascular system, as well as to imaging anatomic spaces within organs, such as the cavities of the heart, including the atria and ventricles. It will also be understood that the methods and apparatus will find applicability to imaging within the esophagus (e.g., transesophegeal echocardiography), the urethra, the uterus, etc.

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The apparatus of the invention includes both an ultrasound imaging catheter system and a catheter tracking system. The ultrasound imaging system generally is provided in the form of a conventional intraluminal catheter having ultrasound imaging capabilities. For details on the general design and construction of such catheters, the reader is directed to Yock, U.S. Patent Nos. 4,794,931, 5,000,185, and 5,313,949; Sieben et al., U.S. Patent Nos. 5,243,988, and 5,353,798; Crowley et al., U.S. Patent No. 4,951,677; Pomeranz, U.S. Patent No. 5,095,911, Griffith et al., U.S. Patent No. 4,841,977, Maroney et al., U.S. Patent No. 5,373,849, Bom et al., U.S. Patent No. 5,176,141, Lancee et al., U.S. Patent No. 5,240,003, Lancee et al., U.S. Patent No. 5,375,602, Gardineer et al., U.S. Patent No. 5,373,845, Seward et al., Mayo Clinic Proceedings 71(7):629-635 (1996), Packer et al., Cardiostim Conference 833 (1994), "Ultrasound Cardioscopy," Eur.J.C.P.E. 4(2):193 (June 1994), Eberle et al., U.S. Patent No. 5,453,575, Eberle et al., U.S. Patent No. 5,368,037, Eberle et al., U.S. Patent No. 5,183,048, Eberle et al., U.S. Patent No. 5,167,233, Eberle 15 et al., U.S. Patent No. 4,917,097, Eberle et al., U.S. Patent No. 5,135,486, and other references well known in the art relating to intraluminal ultrasound devices and modalities. The catheter will typically have proximal and distal regions, and will include an imaging tip located in the distal region. Such catheters have an ability to obtain echographic images of the area surrounding the imaging tip when 20 located in a region of interest inside the body of a patient. The catheter, and its associated electronic circuitry, will also be capable of defining the position of the catheter axis with respect to each echographic data set obtained in the region of interest.

The catheter tracking system generally includes at least one ultrasound transducer mounted adjacent the imaging tip of the catheter, the signal of which is used to track the location and/or angulation of the imaging tip during movement. In the reception mode, the signal used to track location of the imaging tip is electric, while in the emission mode the signal will be acoustic. The movement is usually pull-back, but also including lateral movement in all six degrees of freedom ((x,y,z) and three angles). In the remaining disclosure we

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shall typically discuss pull-back alone, but it will be understood that all other forms of movement are contemplated including tip deflection within a steerable catheter. The tracking transducer operates in two modes. In the reception mode, the signal used to track location of the imaging tip is electric, while in the emission mode the signal will be acoustic. In another embodiment, a pair of transducers mark the location of the imaging tip during pull-back. The pair of closely spaced transducers define a line which approximates the tangent to the curve defined by the catheter at that point. Thus, angulation of the catheter is determined by finding the line through the positions of at least two transducers adjacent the imaging tip as an approximation of the catheter tangent. Where only a single transducer marks the location of the catheter tip during pull-back, the catheter tangent is approximated by the line defined by two sequential positions of the marker transducer during pull-back.

The catheter tracking system further includes a number of transducers located away from the intraluminal ultrasound (ILUS) catheter, 15 generally two or more, more preferably three or more, more preferably four or more. These transducers form a reference frame, and they may be located internally and/or externally of the patient. The tracking system further includes electronic circuitry for activating certain transducers to generate ultrasound signals for reception by certain other ultrasound transducers. The system also includes circuitry for measuring elapsed time between generation of the ultrasound signals and reception by respective other ultrasound transducers. Moreover, the tracking system will include electronic circuitry for calculating positions of the frame transducers and catheter tip transducers relative to each other using known velocity of ultrasound waves and triangulation, and using measured elapsed times. 25 This tracking system allows the user to determine the 3D coordinates (x, y, z) of each marker transducer at successive times during catheter pull-back. An example of a catheter tracking system, and its method of use to determine 3D coordinates (x, y, z) of a moving point, are described in Smith et al., U.S. Patent No. 5,515.853, the contents of which are incorporated herein by reference, and will not be further discussed here.

The methods of the invention will generally include a step of positioning the ILUS catheter imaging tip within the patient at a region of interest. The ILUS catheter may then be operated to obtain a series of echographic images during catheter pull-back. In a preferred embodiment, the pull-back is an ECG-gated pull-back as disclosed in Roelandt et al., Circulation 90(2):1044-1055 (1994) and Laban et al., Thorax Center, University Hospital, Rotterdam, Netherlands, "ANGUS: A new Approach to Three-dimensional Reconstruction of Coronary Vessels by Combined Use of Angiography and Intravascular Ultrasound." During acquisition of each echographic data set, the position of the catheter axis with respect to the data set is determined and recorded. This step is done by the imaging catheter. Moreover, the 3D coordinates of the catheter tip are also determined and recorded for each echographic data set. This step is done by the tracking system. The recorded positions of the catheter tip are used to calculate a catheter pull-back trajectory in 3D space, taking into account a correction for the imaging transducer not being positioned at exactly the location of the one or more marker transducers. The echographic images are stacked around the catheter trajectory. This step is the 3D reconstruction. The origin of a first echographic data set is placed at the first recorded position, and then each subsequent image is positioned at its respective distance from the first image. During this positioning step, it is preferable to align the recorded catheter axis with the pull-back trajectory so that each image data set has the proper angle of orientation relative to the pull-back trajectory.

#### **Brief Description of Drawings**

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- Fig. 1 depicts a human heart as a site for use of the method and apparatus disclosed herein;
  - Fig. 2 depicts an exploded view of a region of the coronary arteries having an ILUS catheter positioned in a region of interest;
- Fig. 3 depicts a pull-back of an ILUS catheter having one omni-30 directional tracking transducer;

Fig. 4 depicts lateral movement which may occur during pull-back of the ILUS catheter shown in Fig. 3;

Fig. 5 depicts a pull-back of an ILUS catheter having two omnidirectional tracking transducers;

Fig. 6A depicts the ILUS catheter of Fig. 5 positioned within a linear region of a vessel;

Fig. 6B depicts the ILUS catheter of Fig. 5 positioned within a highly curved region of a vessel;

Fig. 7 depicts a patient having a catheter tracking system positioned for use and an automated pull-back device mounted on the ILUS catheter;

Fig. 8 depicts a schematic block diagram of an optical coherence domain reflectometer; and

Fig. 9 depicts an embodiment of an optical coherence tomography catheter module.

### 15 Detailed Description

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The methods disclosed herein are applicable to ultrasound imaging of the coronary arteries as depicted in Fig. 1, or to any body cavity where the image is to be obtained over a region where the position trajectory of the catheter may vary. With reference to Fig. 1, heart 99 includes coronary arteries 98 which follow a tortuous path along the surface of the heart, having curvatures in many locations. Fig. 2 shows an exploded view of curvature 97, having an ILUS catheter disposed within a region of interest therein. Catheter 21 has distal end 22 and a proximal end (not shown), and is generally designed in accordance with imaging catheters known in the art. The catheter thus includes an intraluminal ultrasound imaging system capable of obtaining echographic images of the surrounding of catheter tip 22. The imaging system includes transducer 23 and its associated electronics for displaying an echographic data set, e.g., obtained by rotating transducer 23 over a 360-degree path 24 about distal tip 22 of catheter 21 to scan the vessel interior, or by a sector scan which makes a 60 or 90 degree scan of the vessel interior. In an alternative embodiment, transducer 23 is replaced by

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a phased array of transducers as disclosed in Griffith et al., U.S. Patent No. 4,841,977. Scanning of the vessel interior is repeated many times during pull-back to obtain a plurality of echographic data sets taken at a sequence of positions 27 within vessel 98.

In one embodiment, each echographic data set obtained during pull-back comprises a transverse or cross-sectional image of the vessel at the point of the image, as shown in Fig. 2. In another embodiment, each image represents essentially a conical plane having its top at the position of the imaging transducer. In this case, the top angle of the conical plane is usually large, and typically 150-170 degrees. In another embodiment, each echographic data set represents essentially a 3D cloud having its origin at the position of the ultrasound imaging transducer.

The apparatus herein further includes a catheter tracking system which enables real-time determination of the 3D coordinates and angulation of the 15 catheter imaging tip during use within a body. The tracking system includes at least one transducer 25 mounted on the catheter and typically adjacent the imaging tip 23, as shown in Fig. 2. Transducer 25 can be mounted either proximal or distal to scanning transducer 23. However, a distal mount may lead to image artifacts because of transducer leads which cross the image plane. In another 20 embodiment, catheter 21 includes two tracking transducers 25 and 26 spaced by a short distance. Optimum spacing is determined by considering two competing parameters; accuracy of angulation measurement and percent error due to limits on resolution. Tracking system resolution is the limiting factor in determining how close the two transducers can be placed. It is desired to have the two transducers placed as close as possible in order to optimize the accuracy of the angulation. However, because the currently available resolution permits determination of position to within about 1 mm, in order to minimize the percent error due to the limits on resolution, it is best to space the tracking transducers by greater than 5 mm, more preferably greater than 7 mm, more preferably greater than 9 mm, and most preferably at or greater than about 10 mm. In any case, it is best to limit the spacing of the tracking transducers to no greater than about 15 mm or less, more

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preferably no greater than about 12 mm or less, more preferably no greater than about 10 mm or less, with about a 10 mm spacing being most preferred.

It is desirable to be able to calculate the tangent to the catheter centerline or to the trajectory of the imaging transducer at each point where

5 echographic data is acquired. In one embodiment, where two or more tracking transducers are employed, the tangent is approximated by the line defined by the two or more points determined by the location of the tracking transducers. In another embodiment, where only one tracking transducer is employed, the tangent is approximated by the line through two points determined by the successive

6 locations of the tracking transducer at two positions during pull-back. The tangent, or angulation, once determined, provides the proper angle of placement of each echographic data set since each data set may be placed so that the recorded catheter axis for each data set coincides with the tangent at the point where the echographic data set was recorded. Numerous averaging techniques known in the art can be used to smooth large deviations in the obtained trajectory caused by stochastic errors or resolution deficiency.

The catheter tracking system also includes a number of transducers located away from the ILUS catheter which collectively define a reference frame. It is desired to have at least three transducers away from the catheter and in the reference frame so that the tracking transducer and the reference frame transducers are not all included in one plane. The design and use of a catheter tracking system is fully discussed in Smith et al., U.S. Patent No. 5,515,853.

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An ILUS catheter and a tracking system as disclosed herein is shown deployed in a patient in Fig. 7. The tracking system includes reference frame transducers disposed within chest harness 101. Catheter 21 enters the patient through the femoral artery and is positioned within a region of interest, e.g., within the coronary arteries. The proximal end of catheter 21 includes handle 102 which is coupled to an automatic pull-back device (APD) 103. Processing system 104 receives electronic input from the reference frame transducers through wires 105, from the tracking transducers through wires 106,

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from the ILUS catheter imaging system through wires 107, and from the APD through wires 108.

In use, the ILUS catheter is deployed according to procedures well known in the art. For imaging in the coronary artery, the catheter is inserted through an incision in the femoral artery (Fig. 7) and is advanced upwardly through the descending aorta, typically with assistance from a guiding catheter, until it crosses the aortic arch and reaches the coronary arteries. Where the region of interest lies within a different vessel or organ, the means for entry will obviously differ, but will follow established techniques known in the art. The ILUS catheter is positioned so that the imaging tip lies within a region of interest inside the body of a patient, as depicted in Fig. 2. The catheter imaging system is then carried through a pull-back sequence, optionally using an automated pull-back device as disclosed by Webler et al., U.S. Patent Nos. 5,361,768 and 5,485,846, and Ream, U.S. Application Serial No. 08/722,325, filed 15 September 27, 1996, and Ream, U.S. Application Serial No. 08/721,433, filed September 27, 1996. During pull-back, a series of echographic data sets is obtained, each of which will provide the necessary input to produce an image which can be displayed according to processes and using electronic equipment well known in the art.

At the time each image is captured, the position of the catheter axis with respect to each echographic data set obtained during pull-back is defined by the position of the transducer, and is therefore known. During pull-back of the catheter imaging tip, it is also desired to record the position (x, y, z) and the time at each interval for which data is recorded, according to the method of U.S. Patent No. 5,515,853. From this information, it is possible to calculate the velocity of catheter tip movement and to record this information as well. Moreover, it is desired to determine and record the angulation in 3D space of the imaging tip for each image using the coordinates (x, y, z) of the one or more tracking transducers as discussed above.

The coordinates (x, y, z) of each point of image acquisition along the catheter pull-back path are then used in conjunction with the time data to

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reconstruct a 3D image by stacking the echographic images around the catheter pull-back trajectory. The origin of the first image is placed at a first recorded position. The next image is then positioned at its respective distance from the first image, and this process is repeated until all images within the region of interest 5 have been placed along the pull-back trajectory. Each echographic data set is adjusted so that the catheter axis recorded for that data set is aligned with the catheter pull-back trajectory. In this manner, for cross-sectional scanning, each echographic data set is oriented at a substantially 90-degree angle to the longitudinal axis of the ILUS catheter. Linear interpolation is performed between digitized adjacent image sets, resulting in a volumetric (voxel) data set, as described in Evans et al., Circulation 93:567-576 (1996), incorporated herein by reference. The voxel data set can be resliced, creating a new series of 2D frames. 3D images can be created by processing the data with algorithms developed specifically for voxel-based image display (Sonoview, Pura Labs). The resulting images are displayed on a workstation for display and analysis.

Where the echographic data sets are 3D clouds, each cloud may overlap at its boundaries with the adjacent image cloud. Thus, it may be desired to make certain adjustments in the echographic data to eliminate distortions which may occur at the boundaries between overlapping images. Moreover, error may occur due to what is known as "sock rotation," which refers to the rotational orientation of each echographic data set relative to a fixed reference. We adjust for this error by using anatomic landmarks within the vessel or cavity being imaged, so that the rotational orientation of each data set is adjusted relative to the placement of that landmark.

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In another embodiment, adjustment may be made for image rotation caused by torsion of the catheter during pull-back due to bends in different planes. This typically shows up as image rotation which may distort a reconstructed image if not corrected for. This distortion is referred to as "twist," and arises because the images are rotated to a different degree around their origin along their path during pull-back. This phenomenon, and a solution to correct for it, is described in Laban et al., Thorax Center, University Hospital, Rotterdam, Netherlands,

"ANGUS: A new Approach to Three-dimensional Reconstruction of Coronary Vessels by Combined Use of Angiography and Intravascular Ultrasound," and will not be further discussed here in the interest of brevity.

In another embodiment, the catheter tip position is recorded during pull-back by using an electromagnetic position and orientation determining system as described by Aretz et al., International Journal of Cardiac Imaging 6:231-237 (1991), Acker et al., International Application No. PCT/US94/11298 (USSN 08/132,479, filed October 6, 1993), and Ben-Haim et al., International Application No. PCT/US95/01103 (USSN 08/293,859, filed April 19, 1994), incorporated herein by reference.

Example 1: 3D Reconstruction Using Catheter with One Omni-Directional Tracking Transducer

Stacking of images to obtain 3D reconstruction is accomplished using a catheter with one tracking transducer by calculating an approximate

15 tangent to the pull-back trajectory using two successive points for the tracking transducer, as depicted in Fig. 3. Transverse images 52 and 53 are obtained during pull-back 57 along trajectory 51. At a first point in time,  $t=t_1$ , the tracking transducer lies at position 1, corresponding to point 54. The image plane 52 is displaced by distance 56 (s) from position 1, and this displacement s corresponds to the distance between a distal tracking transducer and a slightly proximal scanning transducer. At a second point in time,  $t=t_2$ , the tracking transducer lies at position 2, corresponding to point 55. The image plane 53 is again displaced by distance s from position 2.

Thus, at position 1 ( $t=t_1$ ), the tip coordinates are given by ( $x_1$ ,  $y_1$ ,  $z_1$ ), while at position 2 ( $t=t_2$ ), the tip coordinates are given by ( $x_2$ ,  $y_2$ ,  $z_2$ ). The direction and the length of the vector between position 1 and position 2 is given by the vector

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The direction and the length of the vector between position 1 and the image plane 52 is given by the vector

$$\frac{s}{\sqrt{(x_2-x_1)^2+(y_2-y_1)^2+(z_2-z_1)^2}}(x_2-x_1,y_2-y_1,z_2-z_1)$$

The normal vector on image plane 52 is

$$(n_1, n_2, n_3) = \frac{(x_2 - x_1, y_2 - y_1, z_2 - z_1)}{\sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}}$$

This vector positions image plane 52 at a 90° angle to the tangent, the direction of which is approximated by the direction of the vector between position 1 and position 2. The mathematical description of image plan 52 is therefore defined by

$$n_{1}x + n_{2}y + n_{3}z = n_{1}\left(x_{1} + \frac{s(x_{2}-x_{1})}{\sqrt{(x_{2}-x_{1})^{2} + (y_{2}-y_{1})^{2} + (z_{2}-z_{1})^{2}}}\right) +$$

$$n_{2}\left(y_{1} + \frac{s(y_{2}-y_{1})}{\sqrt{(x_{2}-x_{1})^{2} + (y_{2}-y_{1})^{2} + (z_{2}-z_{1})^{2}}}\right) +$$

$$n_{3}\left(z_{1} + \frac{s(z_{2}-z_{1})}{\sqrt{(x_{2}-x_{1})^{2} + (y_{2}-y_{1})^{2} + (z_{2}-z_{1})^{2}}}\right)$$

Therefore, in reconstruction, the coordinates of the origin are given

by

$$\begin{pmatrix} x_1 + \frac{s(x_2 - x_1)}{\sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}} \end{pmatrix},$$

$$\begin{pmatrix} y_1 + \frac{s(y_2 - y_1)}{\sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}} \end{pmatrix},$$

$$\begin{pmatrix} z_1 + \frac{s(z_2 - z_1)}{\sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}} \end{pmatrix},$$

and the angulation of the plane is defined by its normal vector  $(n_1, n_2, n_3)$ . Image plane 53 is defined analogously after definition of a position 3, by substitution  $1\rightarrow 2$  and  $2\rightarrow 3$  in  $(x_1, y_1, z_1)$  and  $(x_2, y_2, z_2)$ .

It will be understood that this system and method of calculation has

a potential for significant error if the pull-back is not done in line with the
catheter axis at the catheter tip location. This error is therefore likely to occur
where there is substantial lateral movement during pull-back, such as would occur
in an anatomic cavity within an organ (e.g., the chambers of the heart). This
error is illustrated in Fig. 4 where it can be seen that, for a pull-back starting at

position 54, the entire trajectory is displaced by lateral movement 57'. Thus,
while the real image plane should be calculated as shown by plane 52, an assumed
image plane 58 is generated instead, resulting in a substantial angulation error 59
between the real and assumed image planes. Moreover, this angulation error
causes error 60 to occur in positioning the origin of the image.

15 Example 2: 3D Reconstruction Using Catheter With Two Omni-Directional Tracking Transducers

Stacking of images to obtain 3D reconstruction is accomplished using a catheter with two tracking transducers by calculating an approximate tangent to the pull-back trajectory using the line between the two tracking trans-

ducers at the point in time when echographic image acquisition occurs, as depicted in Fig. 5. Transverse image 52 is obtained at time  $t=t_1$  during pull-back along trajectory 51. At  $t=t_1$ , the first tracking transducer (transducer 1) lies at point 54' (position 1) while the second tracking transducer (transducer 2) lies at point 55' (position 2), separated by distance  $\ell$  corresponding to gap 61. Image plane 52 is displaced by distance 56 (s) from position 1, as described in Example 1.

Thus, at  $t_1$ , the tip coordinates for transducer 1 are given by  $(x_1, y_1, z_1)$ , while the tip coordinates for transducer 2 are given by  $(x_2, y_2, z_2)$ . The distance between transducers 1 and 2 is known and measured to be

$$\ell - \sqrt{(x_2-x_1)^2 + (y_2-y_1)^2 + (z_2-z_1)^2}$$

10 and the image plane is positioned at distance s from transducer 1.

The normal vector on image plane 52 is

$$(n_1, n_2, n_3) = \frac{(x_2 - x_1, y_2 - y_1, z_2 - z_1)}{\sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}}$$

This vector positions image plane 52 at a substantially 90° angle to the tangent, the direction of which is approximated by the direction of the vector between transducers 1 and 2.

The mathematical description of image plane 52 is therefore defined by

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$$n_{1}x + n_{2}y + n_{3}z = n_{1}\left(x_{1} + \frac{s(x_{2} - x_{1})}{\sqrt{(x_{2} - x_{1})^{2} + (y_{2} - y_{1})^{2} + (z_{2} - z_{1})^{2}}}\right) +$$

$$n_{2}\left(y_{1} + \frac{s(y_{2} - y_{1})}{\sqrt{(x_{2} - x_{1})^{2} + (y_{2} - y_{1})^{2} + (z_{2} - z_{1})^{2}}}\right) +$$

$$n_{3}\left(z_{1} + \frac{s(z_{2} - z_{1})}{\sqrt{(x_{2} - x_{1})^{2} + (y_{2} - y_{1})^{2} + (z_{2} - z_{1})^{2}}}\right)$$

Therefore, in reconstruction, the coordinates of the origin are given

$$\left(x_{1} + \frac{s(x_{2} - x_{1})}{\sqrt{(x_{2} - x_{1})^{2} + (y_{2} - y_{1})^{2} + (z_{2} - z_{1})^{2}}}\right), 
\left(y_{1} + \frac{s(y_{2} - y_{1})}{\sqrt{(x_{2} - x_{1})^{2} + (y_{2} - y_{1})^{2} + (z_{2} - z_{1})^{2}}}\right), 
\left(z_{1} + \frac{s(z_{2} - z_{1})}{\sqrt{(x_{2} - x_{1})^{2} + (y_{2} - y_{1})^{2} + (z_{2} - z_{1})^{2}}}\right)$$

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and the angulation of the plane is defined by its normal vector  $(n_1, n_2, n_3)$ . During pull-back, this determination is repeated at  $t = t_2$  (=  $t_1 + \Delta t$ ), at  $t = t_3$  (=  $t_2 + \Delta t$ ), etc.

It will be understood that this technique assumes that transducers 1 and 2 lie on a straight line with image plane 52 oriented perpendicularly, as shown in Fig. 6A. This assumption may lead to significant error where the catheter has a high degree of curvature between transducers 1 and 2 at any point of echographic data acquisition. This error is illustrated in Fig. 6B where it can be seen that, for an image acquired at t<sub>1</sub>, the tangent is approximated by line 61, while the true

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tangent 62 has a significant displacement therefrom. Thus, while the real image plane should be calculated as shown by plane 52, an assumed image plane 58 is generated instead, resulting in angulation error 59 between the real and assumed image planes. Moreover, this angulation error causes error 60 to occur in positioning the origin of the image.

On the other hand, the use of two tracking transducers prevents error associated with lateral movement which occurs if the pull-back is not done in-line with the catheter axis at the catheter tip location. This is because the tangent to the pull-back trajectory is calculated from coordinates recorded at a single point in time, whereas error due to lateral movement occurs when two successive points for a single tracking transducer are used to calculate the tangent.

In another embodiment the invention makes use of optical coherence tomography (OCT) to image tissue within a body instead of intraluminal ultrasound. OCT is described generally in Swanson et al., U.S. Patent No. 5,321,501, incorporated herein by reference. Referring to Fig. 8, an optical coherence domain reflectometer (OCDR) 200 is shown. The OCDR includes a short coherence length (broad spectral bandwidth) optical source 201 coupled to an optical coupler 202. The other input to coupler 202 is laser 204 generating an optically visible output which is applied to the coupler through a fiber optic path 205. Laser 204 does not contribute to the normal operation of the system and is utilized only to provide a source of visible light for proper alignment with a sample, when the light from diode 201 is in the infrared region and thus not visible. Further details on the construction and operation of the optical coherence domain reflectometer are given in Swanson et al., U.S. Patent No. 5,321,501.

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Fig. 9 illustrates a catheter module which may be utilized for imaging tubular structures 250 such as blood vessels, the esophagus, or the like. Fiber 251 is embedded in inner rotating sheath 252 which is rotatably mounted within an outer sheath 253. Inner sheath 252 has lens 254 at the end of fiber 251 and angled mirrored surface 255. The probe is scanned longitudinally 257 along 30 vessel wall 250, while inner sheath 252 is rotated to scan the vessel wall in a second dimension. Scanning in the depth dimension to provide a

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three-dimensional scan may be achieved by one of the techniques described in Swanson et al., U.S. Patent No. 5,321,501.

Although the foregoing invention has, for purposes of clarity of understanding, been described in some detail by way of illustration and example, it will be obvious that certain changes and modifications may be practiced which will still fall within the scope of the appended claims.

#### WHAT IS CLAIMED IS:

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1. A method for imaging an organ, lumen, or other internal structure within a body of a patient to obtain three-dimensional reconstruction of a region of interest of the organ, lumen, or other internal structure, said method comprising the steps of:

providing an imaging system which includes a catheter imaging tip;

providing a catheter tracking system comprising at least one
tracking element mounted adjacent to the catheter imaging tip, and a plurality of
reference frame elements located away from the catheter imaging tip;

positioning the catheter imaging tip within the region of interest within the organ, lumen, or other internal structure;

obtaining a plurality of images of the surrounding of the catheter imaging tip during movement of the catheter imaging tip using the imaging system;

recording, relative to each image obtained during movement, the position of a tangent to the catheter at the imaging tip, said tangent providing the local catheter axis;

recording the X,Y,Z coordinates of the image origin in the catheter tip during movement using the catheter tracking system; and

stacking the plurality of images around a curved three-dimensional catheter movement trajectory by positioning the origin of a first image at a first recorded position, and positioning subsequent images at their respective distances from the first image and perpendicular to the catheter axis at each recorded position along the curve.

25 2. The method of Claim 1, wherein the catheter imaging tip is an intraluminal optical coherence tomography probe, and wherein the step of obtaining a plurality of images includes scanning interferometrically the surrounding of the catheter imaging tip.

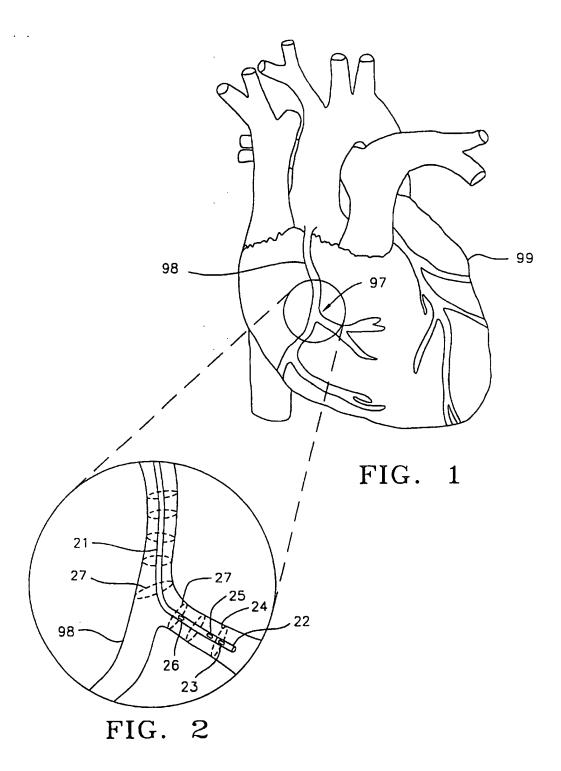
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- 3. The method of Claim 1, wherein the catheter imaging tip is an intraluminal ultrasound imaging probe, and wherein the step of obtaining a plurality of images includes echographically scanning the surrounding of the catheter imaging tip to obtain echographic images, each image corresponding to an echographic data set.
  - 4. The method of Claim 1, wherein the at least one tracking element is an ultrasound transducer mounted adjacent the catheter imaging tip, and wherein the plurality of reference frame elements are ultrasound transducers located away from the catheter imaging tip.
- 5. The method of Claim 4, wherein the catheter tracking system further comprises circuitry for (i) enabling said tracking transducer to generate ultrasound signals for reception by said reference frame transducers, (ii) sequentially measuring elapsed time between generation of said ultrasound signals and reception thereof by said reference frame transducers, and (iii) calculating positions of said frame transducers relative to each other and the position of said tracking transducer relative to said reference frame transducers.
  - 6. The method of Claim 1, wherein the movement of the catheter includes pulling back the catheter imaging tip.
- 7. The method of Claim 1, wherein each image is positioned so that the recorded tangent to the catheter is aligned with an approximate tangent to the catheter movement trajectory.
- 8. The method of Claim 5, further comprising the step of repeating said sequence of generation and reception of ultrasound signals and calculation of transducer positions in order to determine displacement of said transducers and to determine their velocity.

- 9. The method of Claim 7, further comprising the step of determining the catheter tip angulation.
- 10. The method of Claim 9, wherein the catheter tracking system comprises at least two tracking elements mounted adjacent the imaging tip, and the angulation is determined by finding the line through the positions of the at least two tracking elements adjacent to the imaging tip as an approximation of the catheter tip tangent.
  - 11. The method of Claim 10, wherein the two tracking elements are ultrasound transducers.
- 10 12. The method of Claim 9, wherein the angulation is determined by finding the line through two sequential positions of the at least one tracking element.
  - 13. The method of Claim 1, wherein the at least one tracking element is omni-directional.
- 15 14. The method of Claim 1, wherein the reference frame elements are omni-directional.
  - 15. The method of Claim 1, wherein the reference frame elements are located internally of the patient.
- 16. The method of Claim 1, wherein the reference frame elements are located externally of the patient.
  - 17. The method of Claim 1, wherein the step of obtaining a plurality of images includes scanning essentially a cross-sectional plane substantially perpendicular to the catheter axis at the catheter tip.

- 18. The method of Claim 1, wherein the step of obtaining a plurality of images includes scanning essentially a conical surface having its top at the position of the catheter imaging tip and a large top angle.
- 19. The method of Claim 18, wherein the top angle of the conical surface is 150-170 degrees.
  - 20. The method of Claim 3, wherein each echographic data set represents a three-dimensional cloud having its origin at the catheter imaging tip.
  - 21. The method of Claim 1, wherein the at least one tracking element is mounted within 20 mm of the imaging tip.
- 10 22. A catheter imaging system for imaging an organ, lumen, or other internal structure within a body of a patient to obtain accurate three-dimensional reconstruction of a region of interest of the organ, lumen, or other internal structure, said system comprising:
- a catheter having a proximal region, a distal region, and an imaging tip operably disposed within the distal region of the catheter;
  - a catheter tracking system comprising at least one tracking element mounted adjacent to the catheter imaging tip, and a plurality of reference frame elements located away from the catheter imaging tip;
- an automated longitudinal position translator operably coupled to the imaging tip; and
  - a system coupled to the imaging tip, the tracking system, and the automated longitudinal position translator,
- wherein, during operation, the system automatically pulls back the imaging tip while obtaining a plurality of images of the surrounding of the imaging tip and while tracking the position coordinates of the imaging tip during movement.

- 23. The catheter imaging system of Claim 22, further comprising circuitry for (i) enabling said at least one tracking element to generate ultrasound signals for reception by said reference frame elements, (ii) sequentially measuring elapsed time between generation of said ultrasound signals and reception thereof by said reference frame elements, and (iii) calculating positions of said reference frame elements relative to each other and the position of said at least one tracking element relative to said reference frame elements.
  - 24. The catheter imaging system of Claim 23, wherein the at least one tracking element is a transducer, and the reference frame elements are transducers.
- The catheter imaging system of Claim 22, wherein the at least one tracking element is a transducer, and the reference frame elements are transducers.



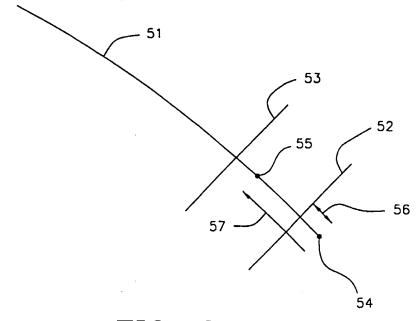
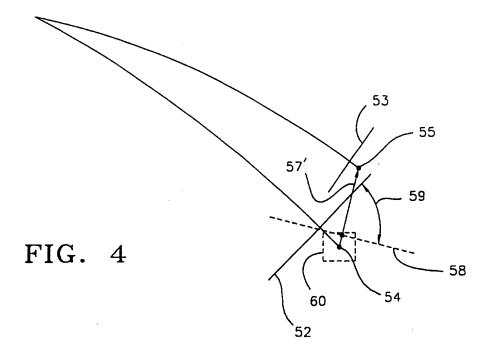
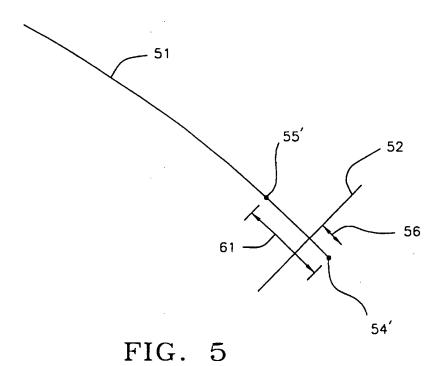


FIG. 3



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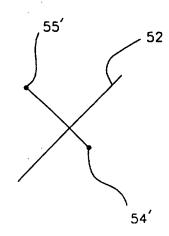


FIG. 6A

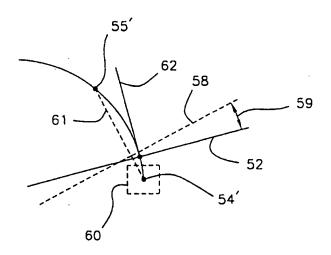


FIG. 6B

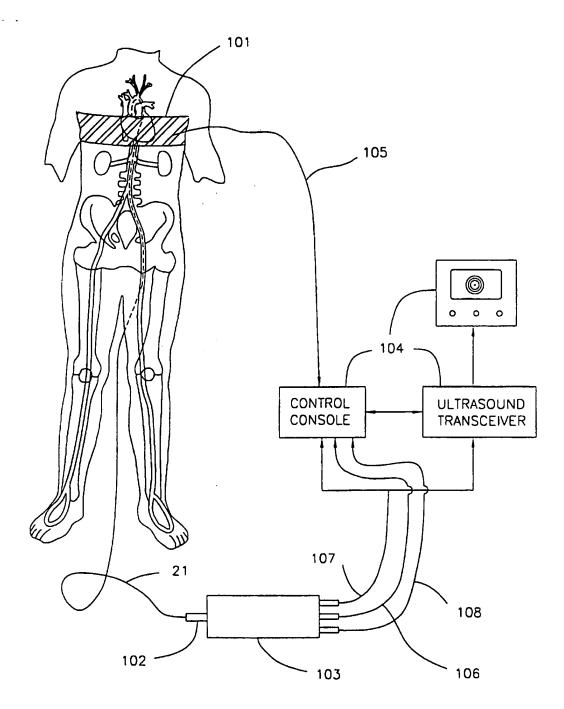
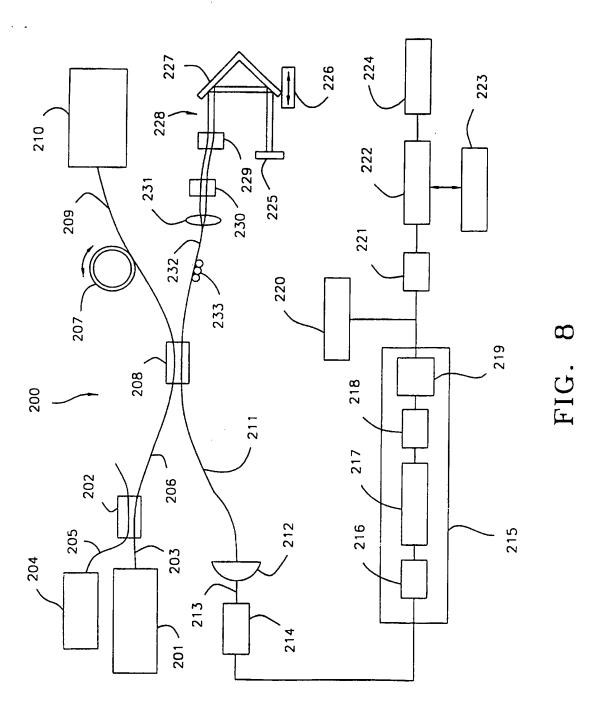
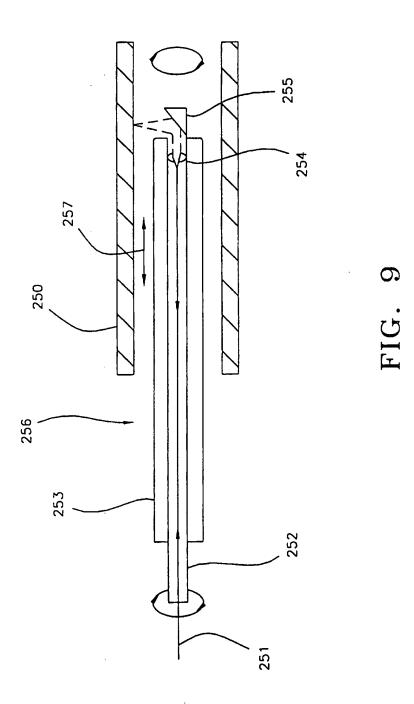


FIG. 7



SUBSTITUTE SHEET (RULE 26)



### INTERNATIONAL SEARCH REPORT

Inter anal Application No PCT/US 97/16455

		P:	CT/US 97/16455		
A. CLASS IPC 6	SIFICATION OF SUBJECT MATTER A61B8/12				
According t	to International Patent Classification (IPC) or to both national classi	fication and IPC			
B. FIELDS	SEARCHED				
Minimum di IPC 6	ocumentation searched iclassification system followed by classific A61B	ation symbolsi			
Documenta	ition searched other than minimum documentation to the extent tha	I such documents are included	in the fields searched		
Electronic	nata base consulted during the international search (name of data	base and, where practical, sear	ch terms used)		
C. DOCUM	ENTS CONSIDERED TO BE RELEVANT				
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Name and m	nailing address of the ISA  European Patient Office, P.B. 5818 Patientiaan 2	Authorized officer			
	NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo ni, Fax: (+31-70) 340-3016	Rieb, K.D.			

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